- We learned how to quantitatively describe the motion of a continuum body including its "internal deformation", which is represented by *strain*.
- In this lecture, we study what is the force associated with the internal deformation and how to incorporate it into the equation of force balance.
- A motion of a body is caused by two kinds of forces: Body and Surface (or contact) force.
 - Gravity governing the free fall of a billiard ball: pure body force.
 - Momentum transfer by collision with another billiard ball: (mostly) surface force.
 - Easy to find examples of deformation of continua by surface forces.



http:

//www.amazon.com/Accoutrements-12021-Stress-Cupcake/dp/B00424LEV4/?tag=cupcakefun-20

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Let's consider a continuous body that is being strained by both body and surface forces.



http://en.wikipedia.org/wiki/Stress_%28mechanics%29

- We need a quantity that represents the internal force arising in response to deformation occurring to a continuum body.
- Such a force should be additive to the body force: i.e., the surface force is also a vector.
- It is useful to consider force "densities":
 ex) The total graviational force is given by the integration of its density:

$$M \mathbf{g} = \int_{V}
ho \mathbf{g} dV$$

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where $\rho \mathbf{g}$ is the force density.

Generally, a body force, F_b is the volume integration of its density, b:

$$\mathbf{F}_b = \int_V \mathbf{b} \ dV$$

Likewise, the surface force (F_s) can also be acquired by integrating its surface density:

$$\mathbf{F}_{s} = \int_{\mathcal{A}} \mathbf{t} \ d\mathbf{A}.$$

We call t, the surface force per area, traction.

With these force densities, we can talk about the local forces acting on a point in the body rather than on the whole body.

- Note that different tractions arise on differently oriented areas even if the "state" of the material is unchanged.
- In particular, the traction is a *linear* function of the normal vector: i.e., we want to have *net traction* by summing up tractions acting on different parts of a surface.
- This property requires the existence of a linear mapping from a normal vector to a traction vector.
- Since a rank 2 tensor can represent such a linear mapping, this relationship hints the idea of stress tensor.
- Let's look at the reasoning leading to the concept of stress tensor more carefully.

Cauchy's tetrahedron:



When no body force is acting, the force equilibrium states

$$\mathbf{t}^n \, d\mathbf{A} - \mathbf{t}^1 \, d\mathbf{A}_1 - \mathbf{t}^2 \, d\mathbf{A}_2 - \mathbf{t}^3 \, d\mathbf{A}_3 = \rho \left(\frac{h}{3} \, d\mathbf{A}\right) \mathbf{a} \quad (1)$$

Since dA_i , $i=1,\ldots,3$ is projection of dA_i ,

$$dA_1 = \mathbf{n} dA \cdot \mathbf{e}_1$$

$$dA_2 = \mathbf{n} dA \cdot \mathbf{e}_2$$

$$dA_3 = \mathbf{n} dA \cdot \mathbf{e}_3$$
(2)

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Substituting (2) into (1), we get

$$\mathbf{t}^n - \mathbf{t}^1(\mathbf{n} \cdot \mathbf{e}_1) - \mathbf{t}^2(\mathbf{n} \cdot \mathbf{e}_2) - \mathbf{t}^3(\mathbf{n} \cdot \mathbf{e}_3) = \rho\left(\frac{h}{3}\right)\mathbf{a}$$
 (3)

Note that *dA* has been cancelled out.

In the limit h → 0, the right hand side is identically zero. Therefore,

$$\mathbf{t}^{n} = \mathbf{t}^{1} \ n_{1} + \mathbf{t}^{2} \ n_{2} + \mathbf{t}^{3} \ n_{3}. \tag{4}$$

Or,

$$t_1^n = t_1^1 n_1 + t_1^2 n_2 + t_1^3 n_3,$$

$$t_2^n = t_2^1 n_1 + t_2^2 n_2 + t_2^3 n_3,$$

$$t_2^n = t_3^1 n_1 + t_3^2 n_2 + t_3^3 n_3.$$
(5)

Eq. (4) further implies that there is a rank 2 tensor, σ, such that

$$\mathbf{t}^n = \boldsymbol{\sigma} \, \mathbf{n},\tag{6}$$

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where the column vectors of σ are \mathbf{t}^i (i = 1...3).

Properties of Cauchy Stress Tensor

- We call the rank 2 tensor σ the *Cauchy stress tensor*.
- Note that all the considerations so far have been made with respect to the *current* (or deformed) configuration.
- When projected along the standard orthonormal basis, {e_a}, we get

$$\mathbf{e}_{a} \cdot \boldsymbol{\sigma} \mathbf{e}_{b} = \sigma_{ab}.$$



$$\mathbf{t}_{e_1} = \boldsymbol{\sigma} \mathbf{e}_1 = \sigma_{11} \mathbf{e}_1 + \sigma_{21} \mathbf{e}_2 + \sigma_{31} \mathbf{e}_3,$$

$$\mathbf{t}_{e_2} = \boldsymbol{\sigma} \mathbf{e}_2 = \sigma_{12} \mathbf{e}_1 + \sigma_{22} \mathbf{e}_2 + \sigma_{32} \mathbf{e}_3,$$

$$\mathbf{t}_{e_3} = \boldsymbol{\sigma} \mathbf{e}_3 = \sigma_{13} \mathbf{e}_1 + \sigma_{23} \mathbf{e}_2 + \sigma_{33} \mathbf{e}_3.$$
(7)

From the relations (7), we can visualize traction components and stress components as in Fig. 3.3 of the handout.

Properties of Cauchy Stress Tensor

- Cauchy stress, σ, is symmetric. For a proof, wait until we get to the balance principles.
- Understand the following concepts and the characteristics of the associated Cauchy stress matrix:

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- Normal and shear stress
- Uni-, bi- and triaxial stress state
- Pure shear stress state
- Hydro(or litho)static stress state
- Plane stress state

Properties of Cauchy Stress Tensor

We make frequent use of *invariants*, *principal stresses* and associated directions.

- Principal stresses and strains and the associated principal directions are mathematically eigenvalues and eigenvectors.
- Review the related maths here:

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https:
//www.khanacademy.org/math/linear-algebra/
alternate-bases#eigen-everything
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► Vector coordinate transformation: $\mathbf{v}' = \mathbf{Q}\mathbf{v}$, where \mathbf{Q} is the forward rotation matrix. For instance, a counterclockwise rotation of a point (represented by the coordinate vector) around the x_3 axis by an angle θ (radian) is represented by the following matrix:

$$\mathbf{Q} = \begin{pmatrix} \cos\theta & -\sin\theta & 0\\ \sin\theta & \cos\theta & 0\\ 0 & 0 & 1 \end{pmatrix}$$

- Note that this rotation is equivalent to the rotation of the reference frame by -θ around the x₃ axis; and thus the rotation of the reference frame by θ is represented by the matrix **Q**^T = **Q**(-θ).
- Now, let's say a vector t is mapped by a rank 2 tensor, σ from another vector n in one coordinate system.

$$\mathbf{t} = \boldsymbol{\sigma} \mathbf{n} \tag{8}$$

- When the coordinate system is rotated by θ, how does the rank 2 tensor transform?
- The transformed vectors and tensors are denoted as primed symbols: t', n' and σ'. Then in the rotated coordinate system,

$$\mathbf{t}' = \boldsymbol{\sigma}' \mathbf{n}' \tag{9}$$

Here, we have t' = Q^Tt and n' = Q^Tn. By plugging these into Eq. (9), we get

$$\mathbf{Q}^T \mathbf{t} = oldsymbol{\sigma}' \mathbf{Q}^T \mathbf{n}$$

Therefore

$$\mathbf{t} = (\mathbf{Q}\boldsymbol{\sigma}'\mathbf{Q}^T)\mathbf{n} \tag{10}$$

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From (8) and (10),

$$oldsymbol{\sigma} = \mathbf{Q} oldsymbol{\sigma}' \mathbf{Q}^{ oldsymbol{7}}$$

Equivalently,

$$\boldsymbol{\sigma}' = \mathbf{Q}^T \boldsymbol{\sigma} \mathbf{Q} \tag{11}$$

In a 2D case (e.g., plane stress), we get the Mohr Transformation:

$$\sigma_{11}' = \sigma_{11} \cos^2 \theta + \sigma_{22} \sin^2 \theta + \sigma_{12} \sin 2\theta \tag{12}$$

$$\sigma_{22}' = \sigma_{11} \sin^2 \theta + \sigma_{22} \cos^2 \theta - \sigma_{12} \sin 2\theta \tag{13}$$

$$\sigma_{12}' = (\sigma_{22} - \sigma_{11}) \sin \theta \cos \theta + \sigma_{12} \cos 2\theta \qquad (14)$$

Using this transformation, you can find the angle of a plane on which normal or shear stress is maximized.

Mohr's circle

Let's rearrange the Mohr transformation equations:

$$\sigma_{11}' = \sigma_{11} \frac{1 + \cos 2\theta}{2} + \sigma_{22} \frac{1 - \cos 2\theta}{2} + \sigma_{12} \sin 2\theta$$

$$\sigma_{22}' = \sigma_{11} \frac{1 - \cos 2\theta}{2} + \sigma_{22} \frac{1 + \cos 2\theta}{2} - \sigma_{12} \sin 2\theta$$

$$\sigma_{12}' = (\sigma_{22} - \sigma_{11}) \frac{\sin 2\theta}{2} + \sigma_{12} \cos 2\theta$$

$$\begin{aligned} \sigma_{11}' &= \frac{\sigma_{11} + \sigma_{22}}{2} + \frac{\sigma_{11} - \sigma_{22}}{2} \cos 2\theta + \sigma_{12} \sin 2\theta \\ \sigma_{22}' &= \frac{\sigma_{11} + \sigma_{22}}{2} - \frac{\sigma_{11} - \sigma_{22}}{2} \cos 2\theta + \sigma_{12} \sin 2\theta \\ \sigma_{12}' &= -\frac{\sigma_{11} - \sigma_{22}}{2} \sin 2\theta + \sigma_{12} \cos 2\theta \end{aligned}$$

$$\sigma_{11}' = \frac{\sigma_{11} + \sigma_{22}}{2} + \frac{\sigma_{11} - \sigma_{22}}{2} \cos 2\theta + \sigma_{12} \sin 2\theta \qquad (15)$$

$$\sigma_{22}' = \frac{\sigma_{11} + \sigma_{22}}{2} - \frac{\sigma_{11} - \sigma_{22}}{2}\cos 2\theta + \sigma_{12}\sin 2\theta \qquad (16)$$

$$\sigma_{12}' = -\frac{\sigma_{11} - \sigma_{22}}{2} \sin 2\theta + \sigma_{12} \cos 2\theta \tag{17}$$

- Find an angle θ at which the shear stress (σ'_{12}) vanishes. The angle is called the *principal angle* and the corresponding normal stresses $(\sigma'_{11} \text{ and } \sigma'_{22})$ is called the *principal stress*.
- Since $\tan(2\theta) = \tan(2\theta + \pi) = \tan(2(\theta + \pi/2)), \theta + \pi/2$ is also a principal angle.
- Find the principal stresses.

Mohr's circle

- Let's assume that we started with the principal axes such that $\sigma_{11} = \sigma_1$, $\sigma_{22} = \sigma_2$ and $\sigma_{12} = 0$.
- After a rotation of the coordinate axes by an arbitrary value of θ, we get the following transformed stress components:

$$\begin{aligned} \sigma_{11}' &= \frac{\sigma_1 + \sigma_2}{2} + \frac{\sigma_1 - \sigma_2}{2}\cos 2\theta = -p + R\cos 2\theta, \\ \sigma_{22}' &= \frac{\sigma_1 + \sigma_2}{2} - \frac{\sigma_1 - \sigma_2}{2}\cos 2\theta = -p - R\cos 2\theta, \\ \sigma_{12}' &= -\frac{\sigma_1 - \sigma_2}{2}\sin 2\theta = -R\sin 2\theta. \end{aligned}$$

One can also realize that

$$(\sigma'_{11} + p)^2 + \sigma'_{12}^2 = R^2,$$

and
 $(\sigma'_{22} + p)^2 + \sigma'_{12}^2 = R^2.$

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Mohr's circle

- In other words, since θ is arbitrary, any transformed stress components must be on a circle centered at -p with a radius R.
- ► This circle is called the **Mohr's circle**.
- ► Be careful with the sign convention. Here, we are assuming the **tension positive** convention and the definition, $p = -\sigma_{kk}/n_{dim}$.
- Let's try to understand Figs. 3.14-18 of the handout.

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